ruble il companison between one superneuter and tow superneuter		
Parameter	VVER600MWwith one	VVER600MW with tow su-
	superheater SH1	perheater SH1+SH2
$G_0 \text{ kg/s}$	933.9	935.8
N _e MW	600	600
p_0 MPa	6	6
$p_c \; \mathrm{MPa}$	0.004	0.004
η_{PP} %	0.325	0.352
η_{npp}^{net} %	0.30	0.335

Table 1. Comparison between one superheater and tow superheater

Scientific adviser: A.V. Vorobyov, Candidate of Technical Sciences, Associate Professor of (SEC I.N. Butakova, ISHE) in TPU.

REFERENCE:

- 1. D.J. Stoker, L.S. Mims, S. Siegel Steam superheat boiling water nuclear reactor United States Patent # 3150052 (September, 1964) Google Scholar
- 2. US Atomic Energy Commission (1962-05-01). "Boiling Nuclear Superheater (BONUS) Power Station: final summary design report". Division of Technical Information (PRWRA-GNEC-6).
- 3. "Boiling Nuclear Superheater Rincón, Puerto Rico". National Toxic Land / Labor Conservation Service. Retrieved 28 June 2019.
- 4. https://aris.iaea.org/PDF/VVER-600(V-498).pdf

Scientific adviser: A.V. Vorobiev, candidate of technical sciences, associate professor of the Scientific and Educational Center I.N. Butakov of the Engineering School of Power Engineering of the Tomsk Polytechnic University

EGYPTIAN NUCLEAR POWER PLANT TURBINE PROJECT

K.R. Ibrahim

National Research Tomsk Polytechnic University Power Engineering School, REC named after I.N. Butakova, group 506и

Introduction

My research object is Established Nuclear Power Plant and Design (VVER-850) With design of Turbine from thermal and hydraulic calculation to design Egyptian nuclear power plant which before it was thermal power plant located at Banha city in Egypt Taking into account Geological area and consumers. Given the great demand for electric energy in Egypt, knowing that 105 million Egyptian citizens live only in an area that does not exceed 9 or 10% of the Egyptian land area. Therefore, a nuclear power plant must be established in the delta region of northern Egypt Because of the recent urban expansion in Egypt in terms of building new cities that need new sources of electricity and a diversity of energy sources.

In this paper, a methodology for thermal schema of nuclear power plant and turbine stage calculation

Description of the research object

At my research object I designed Thermal schema of nuclear power plant and turbine stage calculation High and Low pressure part

With Turbine plant efficiency = 32.7 %, Net block efficiency = 31%.

At Turbine consist five stages for High-pressure cylinder at modern nuclear power plants is two-flow

My nuclear power plant VVER-850 consisting intermediate Separator and superheater with two cylinders of turbine High and Low part with Geometric Profile (P-30-21A)

With (6) regenerative feed water heaters from both type open and closed reheater from side of calculation I found the flow rate and pressure at each point in the scheme



Fig. 1. Scheme of npp with flow rate directions functional dependencies To determining steam flow to a turbine

$$G_0 = \frac{N_e \cdot 10^3}{H_i^{\text{total}} \cdot \eta_M \cdot \eta_g \cdot (1 - \Sigma(\alpha_j \cdot y_j))}, \qquad (1)$$

Where:

 η_m is mechanical efficiency of a steam turbine installation = 0,98.

 η_g is efficiency of generator = 0,99.

 α_i is relative steam consumption in the j-th selection.

 y_i is reproduction factor in each extraction.

N_e is electric power of NPP.

H_i^{total} is total internal heat drops in turbine, kJ/kg.

For Turbine plant efficiency.

$$\eta_{\rm tu} = \frac{N_{\rm e}}{Q_{\rm T}},\tag{3}$$

Where:

N_e is electric power of NPP.

Q_T is Thermal loading of turbine.

Calculation of the axial force on the rotor on the example of the first stage of the cylinder

The axial force acting on the rotor depends on the distribution of the vapor pressure over the surface of the rotor and is found as the sum of all axial forces:

$$R\sum_{i=1}^{n} R_a^i , \qquad (3)$$

Within one stage, the axial force acts on the profile part of the working blades R_a^1 , the disk R_a^2 , the ledges on the rotor between the diaphragms of the adjacent diaphragm seals R_a^3 , on the ledges of the seal R_a^4 .

Calculate the total axial force acting on the fourth unregulated stage.

Calculation results

Turbine plant efficiency:

$$\eta_{\rm tu} = \frac{N_{\rm e}}{Q_{\rm T}} = 32.7 \ \% \,, \tag{4}$$

Efficiency of pipelines connecting a steam generating unit with a turbine:

$$\eta_{\text{pipe}} = \frac{Q_{\text{T}}}{Q_{\text{SG}}} = 0.9965 ,$$
 (5)

Net block efficiency:

$$\eta_{NB} = \eta_{tu} \cdot \eta_{pipe} \cdot \eta_{SG} \cdot (1 - K_{on}) = 0.31 , \qquad (6)$$

Specific flow rate of degraded fuel for the electrical supply at nuclear power plants:

$$b_{ndf} = \frac{0.0537}{\eta_{on}^e} = 0.175 \frac{\text{kg}}{\text{kW} \cdot \text{h}},$$
 (7)

The shaft is considered rigid, since the critical frequency is higher than the operating frequency. The condition must be met for a rigid shaft:

$$n_{cr} \ge (1, 2 - 1, 25) n_{op},$$
 (8)

$$\frac{n_{cr}}{n_{op}} = \frac{11478}{3000} = 3.8\tag{9}$$

The condition is met.

Conclusions

After calculations we found that efficiency of Nuclear Power Plants is acceptable also all conditions is met for all calculation from both sides hydraulic and thermal

The design is based on the latest technologies in nuclear power plants in terms of modern turbines in design

LITERATURE:

- 1. Power plant engineering/by Black & Veatch; Lawrence F. Drbal, managing editor, Patricia Boston, associate editor, Kayla L. Westra, associate editor.
- 2. Nuclear Power Plants. Design and Safety Considerations / editor by J. P. Argyriou. — New York: Nova Science Publishers, Inc., 2012.
- 3. Leyzerovich, Alexander. Wet-Steam Turbines for Nuclear Power Plants / A. Leyzerovich. Tulsa: PennWell, 2005.

Scientific adviser: S.V. Lavrinenko, Candidate of Pedagogical Sciences, associate professor of the Scientific and Educational Center I.N. Butakov of the Engineering School of Power Engineering of the Tomsk Polytechnic University